

[2020 QX1) - Tension]

DSM #8 729 :

$W = \tau \times \theta$ - total angle revolution

$$\tau = \frac{8000}{5250 \text{ sec}} = \frac{8000}{5 \times 2\pi}$$

Now $\phi = \frac{TL}{GJ}$ Torque
 $\frac{TL}{GJ} \rightarrow \frac{TL}{\pi R^4/2}$
 modulus of rigidity

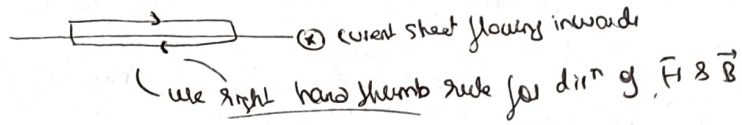
∴ relative shift b/w ends = $L \times \phi$

[2022] via NGP Lec 3

[2022 Q7)

chegg ✓ verified my soln

$(H_1 - H_2) \times \hat{a}_n = \vec{t}_n$ - simple to get from $\oint \vec{B} \cdot d\vec{l} = \mu_0 \vec{I}$
 $(I_3 - I_2)$



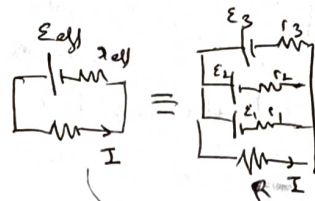
Now $\oint H \cdot dl = I_{enc} \rightarrow (H_1 - H_2)l = kl \rightarrow H_1 - H_2 = k$

also $\nabla \cdot \vec{B} = 0 \rightarrow (B_1)_n = (B_2)_n \rightarrow \mu_{r1} \mu_0 H_1 = \mu_{r2} \mu_0 H_2$

simple soln: $H_1 = 5.5 \hat{a}_x + 6 \hat{a}_y$ A/m

[2022 Q4)

proof of $\frac{\epsilon_{eff}}{\epsilon_0} = \frac{\epsilon_1}{r_1} + \frac{\epsilon_2}{r_2} + \frac{\epsilon_3}{r_3} \dots$ $\epsilon_{eff} = \frac{\epsilon_1 r_2 + \epsilon_2 r_1}{r_1 + r_2}$



$V \sim$ potential across R ($V = IR$)

$V = \epsilon_3 - i_3 r_3 = \epsilon_2 - i_2 r_2 = \epsilon_1 - i_1 r_1 \dots$

$i_1 = \frac{\epsilon_3 - V}{r_3}, i_2 = \frac{\epsilon_2 - V}{r_2} \dots$

$I = \frac{V}{R} = \frac{\epsilon_1}{r_1} + \frac{\epsilon_2}{r_2} + \frac{\epsilon_3}{r_3} \dots - V(\frac{1}{r_1} + \frac{1}{r_2} + \frac{1}{r_3} \dots)$

$V = \epsilon_{eff} - I r_{eff} \rightarrow I = \frac{\epsilon_{eff}}{r_{eff}} - \frac{V}{r_{eff}}$ we compare both eqn

[2022] Q6

Soln verified by chegg. use long derivation to get α & β .

take $k = \alpha + i\beta \rightarrow \nabla^2 E - \mu\sigma \frac{\partial E}{\partial t} - \mu\epsilon \frac{\partial^2 E}{\partial t^2} = 0$

$\nabla^2 E \sim -k^2 E, \frac{\partial E}{\partial t} \rightarrow -j\omega E$ both are -ve sign *

Then $-k^2 - \mu\sigma(-j\omega) - \mu\epsilon(-\omega^2) = 0$

Thus $k^2 = \mu\epsilon\omega^2 + j(\mu\sigma\omega)$
 $= (\alpha^2 - \beta^2) + 2i\alpha\beta$

we solve for α & β ... using Quadratic

Note for both α & β use formula $\rightarrow$ don't use $\beta = \frac{\omega}{v}$ (although answer is almost same only)

Now $v = \frac{c}{\sqrt{\epsilon_r \mu_r}}$ and $H = \frac{k \times E}{\omega \mu}$

$S = \sqrt{\frac{2}{\mu\sigma\omega}}$

< Note in all places $\mu = \mu_0 \mu_r$ >

η - intrinsic impedance

$\sqrt{\frac{j\omega\mu}{\sigma + j\omega\epsilon}} = |\eta| e^{i\theta_\eta}$

$|\eta| = \frac{\sqrt{\mu_0 \epsilon_0}}{[1 + (\frac{\sigma}{\omega\epsilon})^2]^{1/4}}$

and $\tan 2\theta_\eta = \frac{\sigma}{\omega\epsilon}$

[2022 Q3(a1)]

$v = \frac{1}{3}(\bar{a} \cdot \bar{x})c$ $v_{cone} = \frac{1}{3}\pi r^2 h$
 $v_{pyramid} = \frac{1}{3}(\pi r^2 g \cos \theta)(height)$

(But soln of 3(a1) is long & impossible !!)

$F = q\vec{v} \times \vec{B}$
 (note: $F \propto \frac{1}{r^2}$ only for static, coulomb law not for moving charges)
 we can't use $\frac{\mu_0 q^2 v^2}{4\pi r^2}$ - this is for static wire.
 Now $B = \frac{\mu_0}{4\pi} \frac{q\vec{v}}{d^2}$ here not ∞ . Thus use Biot-Savart law
 $F_{21} = qVB = -\frac{\mu_0 q^2 v^2}{4\pi d^2}$

[2022] string EMF



$\epsilon = B \lambda v$

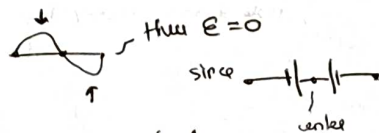
$y = 2a \sin kx \cos \omega t$

$v = \dot{y} = 2a \sin kx \sin \omega t$

$a \sim 3 \text{ mm}$ (max amplitude)

Now integral $\int d\epsilon = \int B v dx$

For 2nd overtone:



$E=0$ also verified by outthink TT channel.

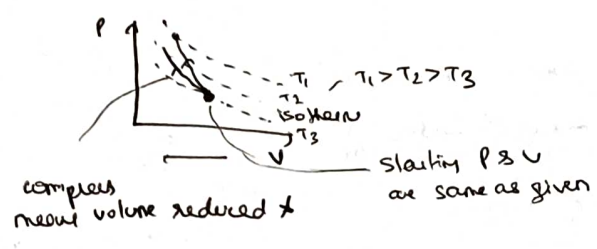
Thermodynamics (2022) PYQ - Q4

(Q1) simple - $dp = \rho g dh$
 and $P = \rho M / RT$
 $P = P_0 e^{-\frac{\rho g h}{RT}} \Rightarrow P = P_0 e^{-\frac{\rho g h}{RT}}$

(Q2) T_f remains fixed since reservoir is large. $\sim$ Thus final Temp is T_f for Body. ($T_i \rightarrow T_f$)
 $OS = C_p \ln \frac{T_f}{T_i} + \frac{Q}{T_f}$
 Now $Q = C_p (T_f - T_i) \sim$ Total heat taken by Body = heat given by reservoir
 Thus $OS = C_p \ln \frac{T_f}{T_i} - C_p \frac{(T_f - T_i)}{T_f}$ since opposite value of Q !

~~Let $T_f = T_i$ then $OS = 0$~~
~~Let $T_f > T_i$ then $OS > 0$~~
~~Let $T_f < T_i$ then $OS < 0$~~
~~Let $T_f = T_i$ then $OS = 0$~~
~~Let $T_f > T_i$ then $OS > 0$~~
~~Let $T_f < T_i$ then $OS < 0$~~
 assume $x = \frac{T_f}{T_i} - 1$
 Now $1 < x < 1$

(Q4) simple: use adiabatic process. There more temp rise overhead
 $\gamma \uparrow \sim$ slope $\uparrow$



(Q5) easy $\times \sim$ given in Q4 DPP soln (easy)

[2020 Q2]
 (easy Q4 soln in DPP easy)

[2019 Q4]
 DPP soln - (1, 8(21 : DOF = 1
 (31 : DOF = 2
 (41 : DOF = 0

GPT: restrictions for -ve temp to be meaningful:

- (1) Two-state or limited energy levels
- (2) Bounded energy levels (i.e. there must be a max energy cutoff)
- (3) Population inversion
- (4) Limited particle count (Gibbs - equilibrium conditions)
- (5) Short time scales

Thus $OS = C_p \left[\ln \frac{T_f}{T_i} - \left(\frac{T_f - T_i}{T_f} \right) \right]$. Now given $\left| \frac{T_f - T_i}{T_f} \right| < 1$
 (1) assume $T_f > T_i \sim$ ~~Let $x = \frac{T_f}{T_i} - 1$~~ $\sim$ Thus $x > 1$

Now $OS = C_p \left[\ln x - \left(1 - \frac{1}{x} \right) \right]$
 at $x = 1 \sim OS = 0 \sim$ Now $\frac{\partial OS}{\partial x} = \frac{1}{x} - \frac{1}{x^2} > 0$ for $x > 1$
 thus +ve slope of $\frac{\partial OS}{\partial x} \sim OS$ is +ve for $x > 1$

(1) assume $T_f < T_i \sim$ Then $OS = C_p \left[\ln \frac{T_f}{T_i} + \left(\frac{T_f - T_i}{T_f} \right) \right]$
 Thus $x < 1$
 This sign same because $\ln \frac{T_f}{T_i}$ will automatically become -ve
 This sign reversed coz we manually had to fix sign of Q .

Thus $OS = C_p \left(\ln x + \left(1 - \frac{1}{x} \right) \right)$
 at $x = 1 \sim OS = 0$
 $\frac{\partial OS}{\partial x} = \frac{1}{x} + \frac{1}{x^2} > 0$ (for $x < 1$)
 Thus in both cases $OS > 0$.
 [extra info: $\log(1+x) = x - \frac{x^2}{2} + \frac{x^3}{3} - \frac{x^4}{4} + \frac{x^5}{5}$
 $e^x = 1 + x + \frac{x^2}{2!} + \frac{x^3}{3!} + \dots$

$\sin x = x - \frac{x^3}{3!} + \frac{x^5}{5!} - \dots$ $\cos x = 1 - \frac{x^2}{2!} + \frac{x^4}{4!} - \dots$

(Q6) we use ~~1st~~ conservation : $n_1 + n_2 = n$
 $\frac{P_1 V_1}{RT_1} + \frac{P_2 V_2}{RT_2} = \frac{PV}{RT}$
 2nd conservation energy :
 $\frac{3}{2} n_1 RT_1 + \frac{3}{2} n_2 RT_2 = \frac{3}{2} n RT$
 $\Rightarrow P_1 V_1 + P_2 V_2 = PV$
 $\Rightarrow P = \frac{P_1 + P_2}{2}$

(Q7) -ve Temp - GBS AM oppend $\sim$ energy in magnetic field
 $\sim$ pop'n inverted
 $\sim$ hole $\rightarrow$ -ve mass (Ragge diffraction)
 various restrictions

To make it easier for using $x \sim x = \frac{T_f - T_i}{T_f}$
 write $C_p \ln \frac{T_f}{T_i} = -C_p \ln \frac{T_i}{T_f} \sim$ Now: $-\ln(1-x) = x + \frac{x^2}{2} + \frac{x^3}{3} + \dots$
 since $\ln(1+x) = x - \frac{x^2}{2} + \frac{x^3}{3} - \dots$
 $-\ln(1-x) = x + \frac{x^2}{2} + \frac{x^3}{3} + \dots$

[2008 Q6]

Chegg soln: $\delta V = \left(\left(\frac{\partial V}{\partial T} \right)_P dT + \left(\frac{\partial V}{\partial P} \right)_T dP \right)$

Then $W = PdV = -P \left(\frac{\partial V}{\partial T} \right)_P dT + P \left(\frac{\partial V}{\partial P} \right)_T dP$
(since isotherms)

Then $W = kV \left(\frac{P_2^2 - P_1^2}{2} \right)$

[2016 Q9(ii)]

viscosity in liquid $\rightarrow$ friction b/w layers
" " gas $\rightarrow$ molecular diffusion
that transports momentum
b/w layers of flow
($\eta = \frac{1}{3} m n \bar{v} \lambda$ (Transport theorem))

[2015 Q3]

$\ln \frac{P_2}{P_1} = \frac{1}{R} \left(\frac{1}{T_1} - \frac{1}{T_2} \right)$

[2015 Q5]

Coefficient of thermal expansion β

$\beta = \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_P$ (verified...)
(volume expansion coefficient)

[2014 Q3]

Throttling is const enthalpy

Now $dQ = 0 \rightarrow dU = -dW$

$dW = P_1 dV_1 - P_2 dV_2$
 $= P_1 V_1 - P_2 V_2$

Then $dU = U_2 - U_1 = P_1 V_1 - P_2 V_2$

$H_1 = U_1 + P_1 V_1 = U_2 + P_2 V_2 = H_2$

[2017 Q3 (ii)]

$T^4 = \frac{300^4 + 200^4}{2}$

Use $\sigma A(T_2^4 - T_1^4) = \sigma A(T_1^4 - T_0^4)$
(emitted) (absorbed)

To T_1 & T_2 are external Temp
Temp body

[2019 Q7] $\sim$ GBG pg 13.8 / 12.34 / 13.2

$Z = \frac{V}{h^3} (2\pi m k T)^{3/2}$ - to find $\langle KE \rangle$ and C_V

proof: $\ln \Omega_{MB} = \ln N! + \sum_i \ln n_i! = \sum_i n_i \ln n_i$
 $= N \ln N - N + \sum_i n_i \ln n_i$

N total particles as in MB distribution

$= N \ln N + \sum_i n_i \ln \frac{n_i}{N}$
 $= N \ln N + \sum_i n_i \ln \frac{1}{N} e^{\beta \epsilon_i}$ since $\frac{n_i}{N} = \frac{g_i e^{-\beta \epsilon_i}}{Z}$

$= N \ln N + \sum_i n_i \ln \frac{1}{N} - \sum_i n_i \ln N + \sum_i n_i \beta \epsilon_i$

$= \sum_i n_i \ln Z + \beta \sum_i \epsilon_i n_i$
 $= N \ln Z + \beta E$

Now $S = k_B \ln \Omega_{MB} = N k_B \ln Z + \beta k_B E$

Then $S = N k_B \ln Z + \beta k_B E = \left(N k_B \ln Z + \frac{U}{T} \right)$

Now $F = U - TS \rightarrow F = -N k_B T \ln Z$

Now $dF = T dS - P dV + \mu dN$
 $= -P dV - S dT$

Then $S = - \left(\frac{\partial F}{\partial T} \right)_V$
 $= - \frac{\partial}{\partial T} (-N k_B T \ln Z)$

$= N k_B \ln Z + N k_B T \frac{\partial}{\partial T} (\ln Z)$

$S = - \frac{F}{T} + N k_B T \frac{\partial}{\partial T} (\ln Z)$

Use $F = U - TS$

Thus $U = N k_B T^2 \frac{\partial}{\partial T} (\ln Z)$

for $P \sim P = \left(- \frac{\partial F}{\partial V} \right)_T = N k_B T \frac{\partial}{\partial V} (\ln Z)$
 $= N k_B T \times \left(\frac{1}{Z} \frac{\partial Z}{\partial V} \right)_T$
 $P = \frac{N k_B T}{Z} \left(\frac{\partial Z}{\partial V} \right)_T$

$\mu = \frac{\partial F}{\partial N} = \frac{\partial}{\partial N} (-N k_B T \ln Z)$

$\mu = -k_B T \ln Z$

Now with $Z = \frac{V}{h^3} (2\pi m k T)^{3/2}$ $\rightarrow U = k_B T^2 \frac{\partial}{\partial T} \ln Z$
 $= \frac{3}{2} N k_B T$

$C_V = \frac{3}{2} N k_B = \frac{3}{2} n R$

(N total particles)

[2019 Q6(c) & 2013 7(b)]

Pointing in a wire

(Topp. com & physicsHub)

$$H = \frac{I}{2\pi r} \quad \text{and} \quad E = \frac{V}{L} = \frac{IR}{L}$$

$$\text{Thus } S = EH = \frac{I^2 R}{2\pi a L} \quad (\text{This is correct})$$

(Wikipedia)

using Gauss law: (assume $\odot$ symmetry)

$$E(r) = \frac{W}{r} \quad \text{Now } V = -\int_{R_1}^{R_2} E \cdot dr$$

$$\text{also } H = \frac{I}{2\pi r} \quad S \propto \text{intensity}$$

$$\text{Thus } S = EH = \frac{W}{r} \cdot \frac{I}{2\pi r} = \frac{WI}{2\pi r^2}$$

$$\text{Now } P_{\text{total}} = \int S \cdot dA = \int S \cdot 2\pi r dr$$

$$= \int_{R_1}^{R_2} \frac{WI}{r^2} \cdot 2\pi r dr$$

"W" was out of focus
 $\ln R_2/R_1$ is fixed constant.
 R_2 & R_1 were used as fixed to find V then 2 points to get value of W

case 2: $m_2 \leq m_1 \rightarrow \cos 2\phi = \frac{m_2}{m_1}$ applicable.

new head-on gives $\phi = 0$

so we need ϕ_{max} with $\phi \neq 0$

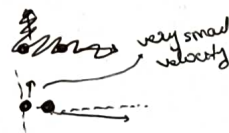
$$\text{then formula is applicable. } \sim \tan \phi_{\text{max}} = \frac{m_2}{\sqrt{m_1^2 - m_2^2}}$$

$$\text{eg: take } m_2 = m_1 \rightarrow \tan \phi = \infty \quad \text{Thus } \phi = 90^\circ$$

This is called

(just mom transferred)

ϕ_{max} more than 90° not possible for $m_1 = m_2$.



My answer is correct, but see pg 6 for same, but simpler.
 (Basically we don't need to put $\phi \rightarrow \phi$, doing $\frac{d}{dt}$ is then same as $\frac{d}{d\phi}$ only....)

But actual easy

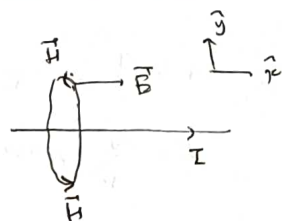
way to get $\phi + \phi' = 90^\circ$

$$\phi = \frac{\phi'}{2} \quad \text{when } m_1 = m_2$$

$$\text{and then } \phi = 90 - \frac{\phi'}{2}$$

$$\phi + \phi' = 90$$

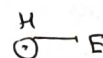
easy proof for $\phi + \phi' = 90^\circ$



here

here $\vec{E}$ is along wire
 since we used $V = E \cdot L$

thus

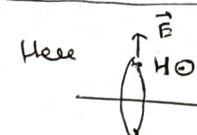


$$S = \vec{E} \times \vec{H}$$

$$\text{Thus } P = S \times A_{\text{area}} = S \times 2\pi a L$$

since this area along $\vec{S}$ using $S = \vec{E} \times \vec{H}$

$$\text{Then power} = VI$$



we use radial $\vec{E}$ and hence

$\vec{S}$ along $-\hat{z}$ dirⁿ

$$\text{thus } A_{\text{area}} = 2\pi r dr$$

$$\text{Thus } P = \int S \cdot dA = VI$$

[2022 Q4(a)]

$h_1 = h_2$ in Bernoulli $\sim$ same height

$$op = \rho gh \quad (\text{h is diff in U-tube})$$

$$v_1^2 - v_2^2 = 2gh \quad \& \quad \phi = Av_1 = Av_2 \quad (\text{eqn of continuity})$$

[2022 Q2(b)] - verify this

don't use internet method of Topp. com & Saadshah since they only use ϕ & not have ϕ & ϕ' as given in question.

$$\text{my method: } \tan \phi = \frac{\sin \phi'}{\frac{m_1}{m_2} + \cos \phi'}$$

$$\text{Now } \phi = 90 - \frac{\phi'}{2} \rightarrow \phi' = 180 - 2\phi$$

$$\text{Thus } \tan \phi = \frac{\sin 2\phi}{\frac{m_1}{m_2} - \cos 2\phi}$$

collect since if we put $m_1 = m_2$ in this, we get $\tan \phi = \cot \phi = \tan(90 - \phi)$

Now assume m_1 & m_2 are fixed.

ϕ & ϕ' can vary in whatever way v_1 & v_2 will accordingly adjust value to make sure $\vec{p}$ is conserved in x & y dirⁿ

eg: take $m_1 = m_2$ - for any value of ϕ , the ball transfer its $\vec{p}$ momentum to 2nd ball in the direction & speed. move 1' since full momentum in original dirⁿ is conserved

also v_1, v_2, ϕ are variable (4) in 3 xⁿ - Thus there is freedom to shift

Thus we want max ϕ .

$$\frac{d}{d\phi} \tan \phi = 0 \quad \sim \text{given } \cos 2\phi = \frac{m_1}{m_2} \frac{m_2}{m_1}$$

$$\text{putting value of } \phi \rightarrow \tan \phi_{\text{max}} = \frac{\sqrt{1 - \frac{m_2^2}{m_1^2}}}{\frac{m_1}{m_2} - \frac{m_2}{m_1}}$$

now case 1 $\rightarrow m_1 < m_2 \rightarrow \cos 2\phi = \frac{m_2}{m_1}$ not applicable then ϕ_{max} anyway 180°

$$\vec{v}_{\text{app}} = \vec{v}_{\text{sep}}$$

such that for elastic collision

$$e = \frac{\text{rel. velocity sep}}{\text{rel. velocity app}} = 1 \quad \text{and } \vec{p} \& \vec{E} \text{ are conserved}$$

$$Q = \frac{\omega_0 L}{R} \text{ where } \omega_0 = \frac{1}{\sqrt{LC}}$$

since we get $c > \omega_0$ in given circuit,

Thus overdamped.

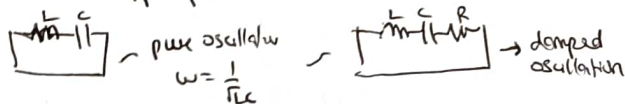


No oscillation! Thus

no resonant frequency.

in underdamped - oscillation exists & we have

ω & ω_0 applicable



$$Q = A_1 e^{-(\gamma \pm \sqrt{\gamma^2 - \omega_0^2})t}$$

for $c > \omega_0$ - overdamped - only exponential terms (no oscillation)

for $c < \omega_0$ - underdamped - we get sine terms & oscillations

$$\omega_d = \sqrt{\omega_0^2 - c^2}$$

outside γ & τ channel:

Also resonance occurs when $\omega_{external} = \omega_0$

in DC - $\omega = 0$ - Thus no resonant frequency

< Resonance always needs AC >

[2013 07] - inhomogeneous (Verify 07)

$$(a) \vec{D} = \epsilon \vec{E} = \epsilon_0 n^2(x, y, z) \vec{E}$$

$$\nabla \cdot \vec{D} = \nabla \cdot (\epsilon_0 n^2 \vec{E}) = 0 \quad (\nabla \cdot \vec{D} = 0)$$

$$\text{Thus } n^2(\nabla \cdot \vec{E}) + \nabla(n^2) \cdot \vec{E} = 0$$

$$\text{Thus } \nabla \cdot \vec{E} = -\frac{1}{n^2} \nabla(n^2) \cdot \vec{E}$$

$$\text{Now } \nabla \times (\nabla \times \vec{E}) = \nabla \times \left(-\frac{1}{n^2} \nabla(n^2) \cdot \vec{E} \right) = -\mu_0 \frac{\partial^2 \vec{D}}{\partial t^2}$$

$$\text{Thus } -\nabla^2 \vec{E} + \nabla(\frac{1}{n^2} \nabla(n^2) \cdot \vec{E}) = -\mu_0 \frac{\partial^2 \vec{D}}{\partial t^2}$$

$$\nabla^2 \vec{E} + \nabla \left(\frac{1}{n^2} \nabla(n^2) \cdot \vec{E} \right) - \mu_0 \epsilon_0 n^2 \frac{\partial^2 \vec{E}}{\partial t^2} = 0$$

$$(b) \nabla \times \vec{H} = \frac{\partial \vec{D}}{\partial t} = \epsilon_0 n^2 \frac{\partial \vec{E}}{\partial t} \quad (\text{since } n^2 \text{ not f of } t)$$

$$\text{Now } \nabla \times (\nabla \times \vec{H}) = \nabla(\nabla \cdot \vec{H}) - \nabla^2 \vec{H} = \epsilon_0 \nabla \times \left(n^2 \frac{\partial \vec{E}}{\partial t} \right)$$

$$\text{Now } \nabla \cdot (f \vec{A}) = f(\nabla \cdot \vec{A}) + \vec{A} \cdot (\nabla f)$$

$$\nabla \times (f \vec{A}) = f(\nabla \times \vec{A}) - \vec{A} \times (\nabla f)$$

$$\text{Thus } -\nabla^2 \vec{H} = \epsilon_0 \left[n^2 \left(\nabla \times \frac{\partial \vec{E}}{\partial t} \right) - \frac{\partial \vec{E}}{\partial t} \times (\nabla n^2) \right]$$

$$= +\epsilon_0 \left[-n^2 \frac{\partial^2 \vec{B}}{\partial t^2} - \frac{\partial}{\partial t} \left[\frac{\partial}{\partial n^2} \right] \times \nabla(n^2) \right]$$

$$-\nabla^2 \vec{H} = \epsilon_0 \left[-n^2 \frac{\partial^2 \vec{B}}{\partial t^2} - \frac{\partial}{\partial t} \times \frac{1}{\epsilon_0 n^2} \nabla(n^2) \right] \quad \text{we took } n^2 \text{ to other side...}$$

$$\text{put } \nabla \times \vec{H} = \frac{\partial \vec{D}}{\partial t}$$

$$\text{Thus } \frac{1}{\epsilon_0} (\nabla \times \vec{H}) \times \left(\frac{1}{n^2} \nabla(n^2) \right) = \vec{H} \left(\nabla \cdot \left(\frac{1}{n^2} \nabla(n^2) \right) \right) - \nabla \left(\vec{H} \cdot \left(\frac{1}{n^2} \nabla(n^2) \right) \right)$$

Let zero - I don't know why

(exact question solved in Soalshak.com & Toppr)

$$\text{Wikipedia} \rightarrow E_{11}' = E''$$

$$B_{11}' = B_{11}$$

$$E_{11}' = \gamma(E_{11} + \vec{v} \times \vec{B})$$

$$B_{11}' = \gamma(B_{11} - \frac{1}{c^2} \vec{v} \times \vec{E})$$

MUG!!

write in formula sheet

remember, as even for normal force:

$$F_{11}' = F_{11} \text{ and } F_{11}' = \gamma F_{11}$$

here we have extra $\vec{v} \times \vec{B}$

and $-\frac{1}{c^2} \vec{v} \times \vec{E} < \text{MUG!!}$

$\vec{B}$ & $\vec{E}$ are full here (no components)

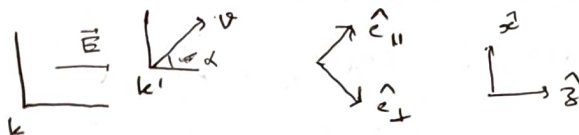
we can also write as:

$$E_x' = E_x \quad E_y' = \gamma(E_y - v B_z) \quad E_z' = \gamma(E_z + v B_y)$$

$$B_x' = B_x \quad B_y' = \gamma(B_y + \frac{v}{c^2} E_z) \quad B_z' = \gamma(B_z - \frac{v}{c^2} E_y)$$

Now in question:

$$E_{11}' = E_{11}, \quad B_{11}' = 0, \quad E_{11}' = \frac{E_{11}}{\sqrt{1-v^2/c^2}}, \quad B_{11}' = \frac{-\vec{v} \times \vec{E}_{11}}{\sqrt{1-v^2/c^2}}$$



$$\text{Let } \vec{E} = (0, 0, E)$$

$$\text{Thus } \vec{v} = (v \sin \alpha, 0, v \cos \alpha)$$

$$\text{Now } \vec{E}_{11}' = (\sin \alpha, 0, \cos \alpha) \quad (\text{unit direction vector of } \vec{E}_{11})$$

$$(a) \text{ Now } E_{11}' = E_{11} \quad \checkmark$$

$$E_{11}' = \frac{E \sin \alpha}{\sqrt{1-v^2/c^2}} \quad \checkmark$$

This is always along $\vec{v}$

$$\text{so } |E'| = E \sqrt{\frac{1-B^2 \cos^2 \alpha}{1-B^2}} \text{ and } \tan \alpha' = \frac{\tan \alpha}{\sqrt{1-v^2/c^2}}$$

$$(b) \vec{B}_{11}' = 0 \text{ and } \vec{B}_{11}' = \frac{\vec{v} \times \vec{E}_{11}}{\sqrt{1-v^2/c^2}} \quad \text{Full } \vec{B} \text{ & } \vec{v} \text{ (no components)}$$

$$= \frac{E v \sin \alpha}{c^2 \sqrt{1-v^2/c^2}}$$

< derivation of Field transformation in AH append

$$\text{Thus we get } \nabla^2 \vec{H} = n^2 \epsilon_0 \frac{\partial^2 \vec{B}}{\partial t^2} - \frac{1}{\epsilon_0} \nabla \left(\frac{1}{n^2} \nabla(n^2) \cdot \vec{H} \right)$$

$$\text{Now } B = \mu_0 H$$

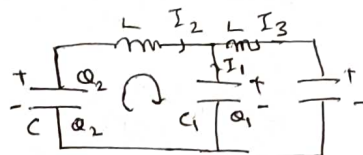
$$\text{Thus } \nabla^2 \vec{B} = \nabla \times \left(\frac{1}{n^2} \nabla(n^2) \cdot \vec{H} \right) - \mu_0 \epsilon_0 n^2 \frac{\partial^2 \vec{H}}{\partial t^2}$$

Thermal Neutron $\rightarrow 3$ day.

[2013]

but use $v_{mp} = \sqrt{\frac{2kT}{m}}$

Then $\lambda = \frac{h}{\sqrt{2mkT}}$



$(I_3 = I_1 + I_2)$

$k_1 = -\frac{1}{LC_1}$ $k = \frac{1}{LC}$

Loop 1 $-\frac{Q_2}{C} - L \frac{dI_2}{dt} - \frac{Q_1}{C_1} = 0$

$\frac{dI_2}{dt} = \frac{Q_2}{LC} - \frac{Q_1}{LC_1}$

$\frac{d^2 I_2}{dt^2} = \frac{1}{LC} I_2 - \frac{1}{LC_1} I_1 = \frac{1}{LC} I_2 - \frac{1}{LC_1} (I_2 - I_3)$
 $= -k I_2 + k_1 (I_3 - I_2)$

[2022 Q2(c)]

system matrix of thick lens

$$\begin{pmatrix} 1 - \frac{p_2 t}{n} & -p_1 - p_2 + \frac{t p_1 p_2}{n} \\ t/n & 1 - \frac{p_1 t}{n} \end{pmatrix} = \begin{pmatrix} a & b \\ c & d \end{pmatrix}$$
 Asymmetric $\rightarrow I_2 = -I_3 \sim \frac{d^2 I_2}{dt^2} = -(k + 2k_1) I_2 \sim \omega_a = \sqrt{k + 2k_1}$

Now symmetric $-I_2 = I_3 \sim \frac{d^2 I_2}{dt^2} = -k I_2 \Rightarrow \omega_s = \sqrt{k}$

Now for a b c d - system matrix and

p_1, p_2 - basically $\propto \Delta v$, we have

$b p_2 + a p_1 p_2 - c p_1 - d = 0$

$(1 - \frac{p_2 t}{n}) p_2 + (p_1 + p_2 - \frac{t p_1 p_2}{n}) p_1 - (1 - \frac{p_1 t}{n}) p_1 - \frac{t}{n} = 0$

$\hookrightarrow$ This is required here formula for thick lens
 $(O \& D_2 \text{ is } \propto \Delta v)$

Thus $\frac{\omega_a}{\omega_s} = \sqrt{\frac{k + 2k_1}{k}}$

But rather soln in my PIAS (3) notes

for thin: here formula is

$\frac{1}{f} - \frac{1}{f} = \frac{1}{f}$

take $\frac{1}{2} = \frac{1}{2_1} + \frac{1}{2_2} + \frac{1}{2_3}$

$z_1 = z_2 = \omega L + \frac{1}{\omega C}$

$z_3 = \frac{1}{\omega C_1}$

symmetric case $\omega_s = \sqrt{2k^2 + k^2}$

now just put

$\omega_a = \frac{1}{\sqrt{LC}} = \frac{1}{\sqrt{LC}} k$

Thus $\frac{\omega_a}{\omega_s} = \frac{k}{\sqrt{2k^2 + k^2}}$

Now $\omega_s = \frac{1}{\sqrt{LC}}$

[2022 Q2(b)]

$\tan \theta = \frac{\sin \theta'}{\cos \theta' + \frac{m_1}{m_2}}$

$\frac{d\theta}{d\theta'} = 0 \rightarrow \cos \theta' = -\frac{m_2}{m_1} \rightarrow \sin \theta' = \sqrt{1 - \frac{m_2^2}{m_1^2}}$

$\cos^2 \theta' + \cos^2 \theta' \left(\frac{m_1}{m_2} \right)^2 + \sin^2 \theta' = 0$

Thus $\tan \theta_{max} = \frac{m_2}{\sqrt{m_1^2 - m_2^2}} \sim \sin \theta_{max} = \frac{m_2}{m_1}$

This answer is verified by my pg 4 soln 3 Toppr.com 3 QY

alternate soln:

$\vec{p}_1 = \vec{p}_1' + \vec{p}_2' \sim \vec{p}_2 = (\vec{p}_1 - \vec{p}_1')$

so $p_2'^2 = p_1'^2 + p_2'^2 - 2 p_1' p_2' \cos \theta$

also $\frac{p_1'^2}{2m_1} = \frac{p_1'^2}{2m_1} + \frac{p_2'^2}{2m_2}$

eliminating p_2' we get:

$0 = p_1'^2 (1 + \frac{m_2}{m_1}) - 2 p_1' p_2' \cos \theta + p_1'^2 (1 - \frac{m_2}{m_1})$

This concludes in p_1' has real soln if:

$4 \cos^2 \theta \geq 4 (1 - \frac{m_2^2}{m_1^2}) \sim \sin \theta_{max} = \frac{m_2}{m_1}$

[2014 Q3] $\rightarrow$ relativistic mirror

now $v' = \frac{1 + \frac{v}{c}}{1 - \frac{v}{c}} v_0$

(soln from website dekarb.phys)

photon $\leftarrow$
 $(\text{from } x = \infty)$

(i) Then $v'' = v' \times \frac{(1 + v/c)}{(1 - v/c)} = v_0 \left(\frac{1 + v/c}{1 - v/c} \right) = v_0 \left(\frac{c + v}{c - v} \right)$ (same like sound $\hookrightarrow$ doppler twice for reflection)

(ii) Now Energy = Intensity

Intensity $\propto E_{\perp}^2$

now $E_{\perp}' = \gamma [E_{\perp} + \vec{v} \times \vec{B}]$ now $|B| \geq \frac{E}{c}$ and in EM wave $\frac{E}{c} = \frac{E_{\perp}}{c}$ all 3 are $\perp$

now $E_{\perp}'' = \gamma [E' - \vec{v} \times \vec{B}']$
 $= \gamma E_{\perp}' (1 + v/c)$
 $= \gamma^2 E_{\perp} (1 + v/c)^2$ 'plus' since v in opp. direction
 $E_{\perp}'' = E_{\perp} \times \frac{(1 + v/c)^2}{(1 - v^2/c^2)} = E_{\perp} \left(\frac{c + v}{c - v} \right)^2$ Both are there $(1 + v/c)$ & $(1 - v^2/c^2)$

Now Intensity $\propto E_{\perp}^2 \Rightarrow$ Thus $\frac{I}{I_0} = \left(\frac{c + v}{c - v} \right)^2$

EM theory of double refraction:

(BJS Pg 501/502)

Anisotropy in diff. dir'n

$$D_x = \epsilon_{11} E_x, D_y = \epsilon_{22} E_y, D_z = \epsilon_{33} E_z$$

$$\vec{D} = \epsilon_0 \vec{E} + \vec{P}, \text{ etc.}$$

now $n_x = \sqrt{\frac{\epsilon_{11}}{\epsilon_0}}, n_y = \sqrt{\frac{\epsilon_{22}}{\epsilon_0}}, n_z = \sqrt{\frac{\epsilon_{33}}{\epsilon_0}}$

Guard rings - Electric field shielding &

- ↳ capacitance reduction
- ↳ noise red'n
- ↳ isolation of components
- ↳ improving accuracy & reliability of measurements.

Guard ring → It is a conducting ring placed around a sensitive component to control electric field and prevent unwanted currents.

They reduce leakage current & parasitic capacitance

They are mainly used in IC's (when C spills over to other components)

↳ conducting ring of copper with low impedance.

Metal detector (mindlab website)

AC voltage - oscillating magnetic field

↳ detector transmits EM field from search coil. any metal object within EM field gets energised and retransmits EM field of it's own which is detected by coil

↳ work on principle of EMF induction

eddy current in metal object create 2ndary magnetic field which opposes original magnetic field. This change is detected by coil.

Artificial dielectric ~ metamaterials created: Nano-structures

↳ work on principle of interaction of EM wave & Nano-structures

↳ this creates novel EM properties which not in Natural material

properties & applications

- Negative refractive Index ~ use in invisibility cloaks
- Superlensing → resolve objects smaller than λ light
- Waveguide & Antenna's ~ high efficiency & low loss
- Absorbers of ^{EM} → stealth technology, EMI shielding
- medical imaging → MRI/PET

artificial dielectric manipulates EM waves at sub-wavelength (nm ~ 10⁻⁹) scales for new properties